

# NUMERICAL MODELLING OF SLURRY TRANSPORT FOR COARSE PARTICLES

Xiuhan Chen, Ting Xiong, Xinzuo Zhang & Sape A. Miedema  
Delft University of Technology, Wuhan University of Technology  
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# Content

- ◆ Goal of Research
- ◆ CFD-DEM Numerical Simulation Method
- ◆ Results and Post-analysis
- ◆ Conclusions

## Goal of Research

- ◆ Observe the flow regimes for transporting coarse particles in the pipe
- ◆ Flow assurance – risk of blockage: the concentration and velocity profile in the pipe
- ◆ Comparison with previous research

# CFD-DEM Numerical Method and verification

1. Fluid phase control equation (CFD part)
2. Solid phase control equation (DEM part)
3. The process of CFD-DEM coupling
4. Verification for accuracy

## 1. Continuity equation and momentum equation

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i} (\rho u_i) = 0$$

$$\frac{\partial}{\partial t} (\rho \xi u_i) + \frac{\partial}{\partial x_j} (\rho \xi u_i u_j) = -\xi \frac{\partial p}{\partial x_i} + \frac{\partial (\xi \tau_{ij})}{\partial x_j} + n_p (F_{\text{drag}} + F_{\text{saffman}} + F_{\text{Magnus}}) + \xi \rho g$$

## 2. k-ε turbulence model

$$\frac{\partial (\rho k)}{\partial t} + \frac{\partial (\rho k u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + G_K + G_b - \rho \varepsilon - Y_M + S_k$$

$$\frac{\partial (\rho g)}{\partial t} + \frac{\partial (\rho \varepsilon u_i)}{\partial x_i} = \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_\varepsilon} \right) \frac{\partial \varepsilon}{\partial x_j} \right] + C_{1\varepsilon} \frac{\varepsilon}{k} (G_K + C_{3\varepsilon} G_b) - C_{2\varepsilon} \rho \frac{\varepsilon^2}{k} + S_\varepsilon$$

Fluid-particle interaction forces:

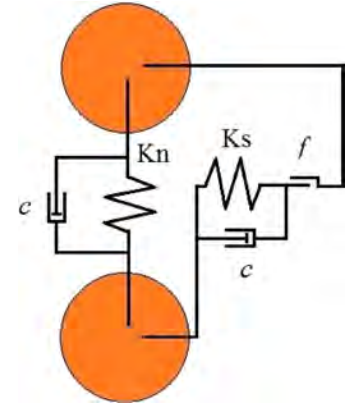
$$\mathbf{F}_{drag} = \frac{1}{8} C_d \rho_f \pi d_p^2 (U^f - U^p) |U^f - U^p| f(e)$$

$$\mathbf{F}_{Magnus} = \frac{1}{2} C_{LM} \pi r^2 \rho_g \frac{\omega_r * u_r}{|\omega_r|}$$

$$\mathbf{F}_{saffman} = 6.46 C_{LS} r^2 \sqrt{\rho_g \eta} \frac{u_r D}{\sqrt{D}}$$

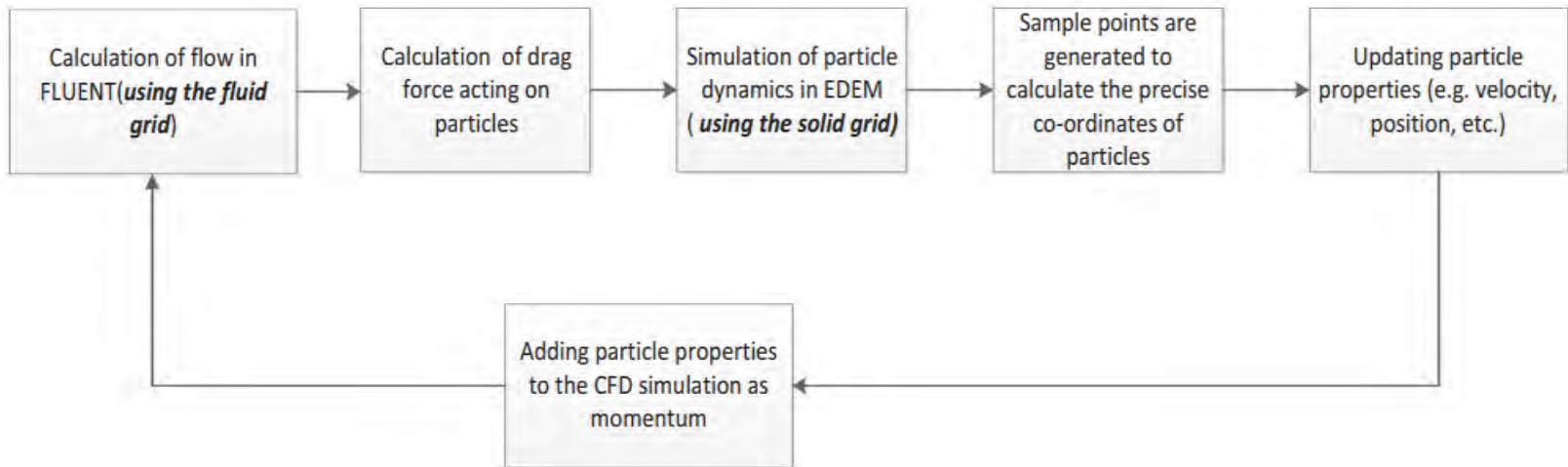
Each individual particle is calculated by using a softball model and the model is described by Newton's equations for translational and rotational motions as follows:

$$m_p \frac{dv_p}{dt} = F_{p-w} + F_{p-p} + F_{drag} + F_{saffman} + F_{Magnus} + m_p g$$



softball model

## The process of using grids in CFD-DEM coupling calculation





## Verification case

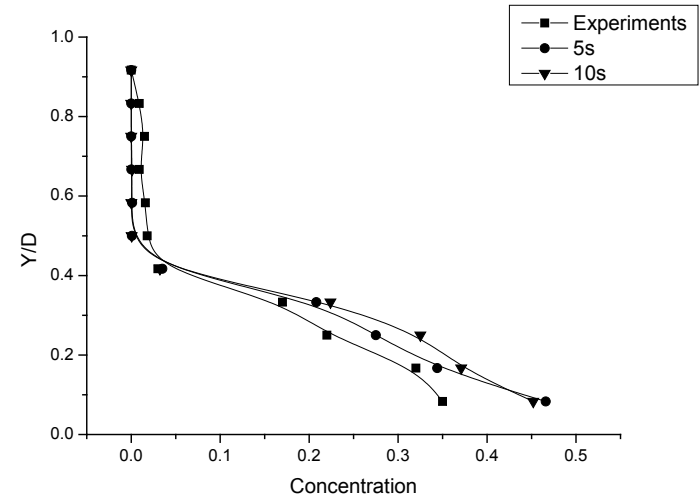
Verification case: experimental data of Vlasak (2014):

$D_p = 0.1$  m  
 $d = 11$  mm  
 $V = 4.1$  m/s  
 $D_p/d \approx 10$

$C_V$  :

- linear at the lower part
- $\approx 0$  at the upper part

The errors are within the allowable range



## Simulation Setup

- I. a horizontal pipe - diameter  $D= 15.24\text{cm}$  and a length of  $7.5\text{m}$ ,
- II. the internal volume of the pipeline is meshed by  $646,720$  CFD fluid cells.
- III. the line speed  $2\text{m/s}$ ,  $5\text{m/s}$  and  $8\text{m/s}$ ,
- IV. the particle size  $d$  is  $10\text{mm}$ ,
- V. input volume concentration  $10\%$ .
- VI. outlet pressure  $\rightarrow$  atmospheric

## **Results & Analysis**

- I. Analysis of the flow regimes at different line speeds**
- II. Concentration distribution of particles**
- III. Velocity distribution of particles**
- IV. Non-spherical coarse particles**

## Analysis of the flow regime at different velocities

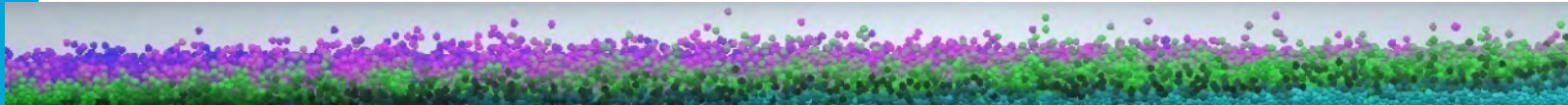
---change of the flow state of the slurry is not a transient phenomenon



(a) Incoming flow from the left:  $V=2 \text{ m}\cdot\text{s}^{-1}$ , fixed bed flow regime (restricted flow state)



(b) Incoming flow from the:  $V=5 \text{ m}\cdot\text{s}^{-1}$ , sliding bed flow regime (sliding friction-dominated flow state)



(c) Incoming flow from the left:  $V=8 \text{ m}\cdot\text{s}^{-1}$ , sliding flow regime (collision-dominated flow state)

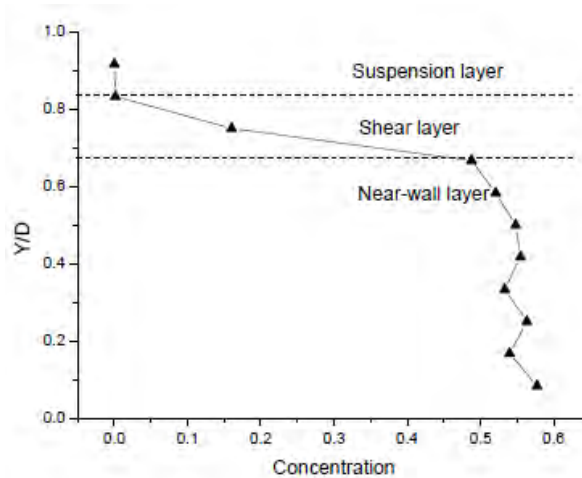


(d) Incoming flow from the left:  $V=10 \text{ m}\cdot\text{s}^{-1}$ , sliding flow regime

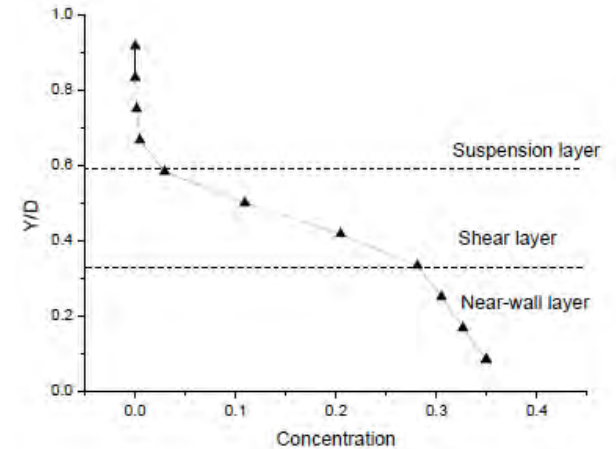
Analytical: SLDV =  $1.9 \text{ m/s}$  (fixed bed to the sliding bed )

LDV =  $3.6 \text{ m/s}$  (the sliding bed to the sliding flow )

## $C_v$ profile

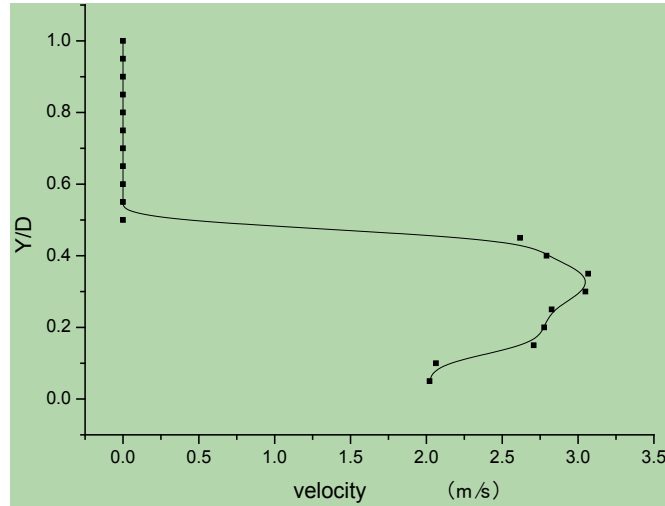


Concentration Profile in the cross-section at  $X = 4\text{m}$  with line speed of  $5\text{m/s}$  (Sliding bed flow regime)

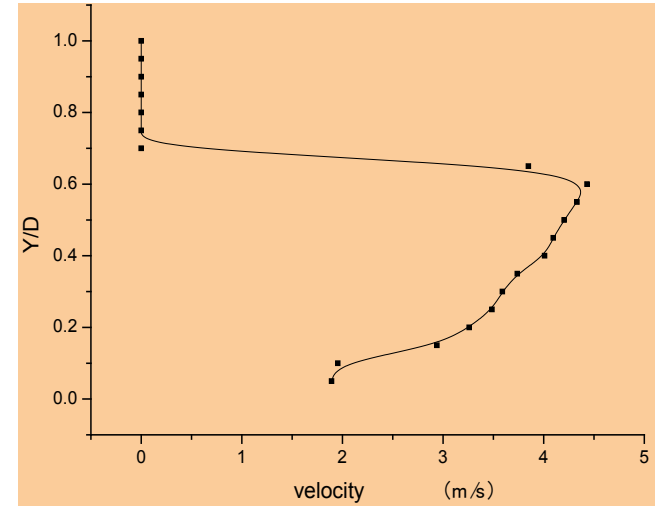


Concentration Profile in the cross-section at  $X = 4\text{m}$  with line speed of  $8\text{m/s}$  (Sliding flow regime)

## Velocity profile of the particles



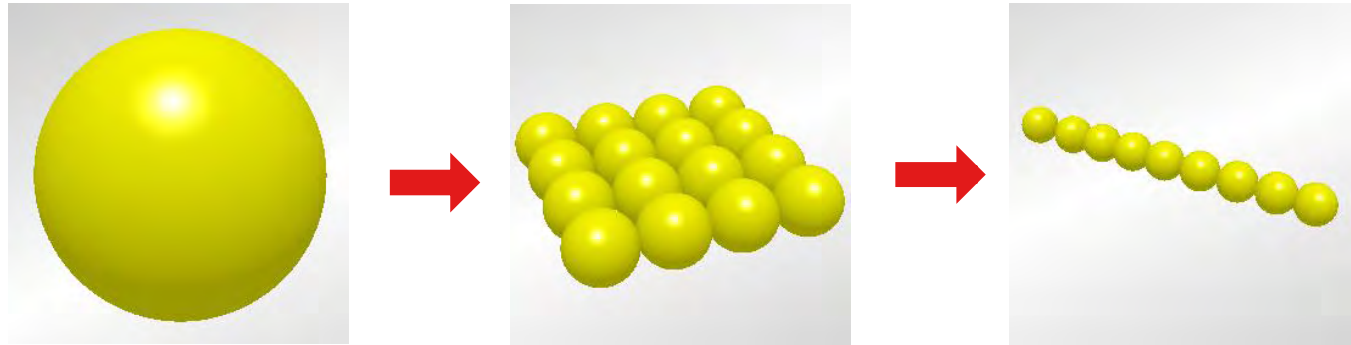
sliding bed regime ( $V=5\text{ m/s}$ )



sliding flow regime ( $V=8\text{ m/s}$ ).

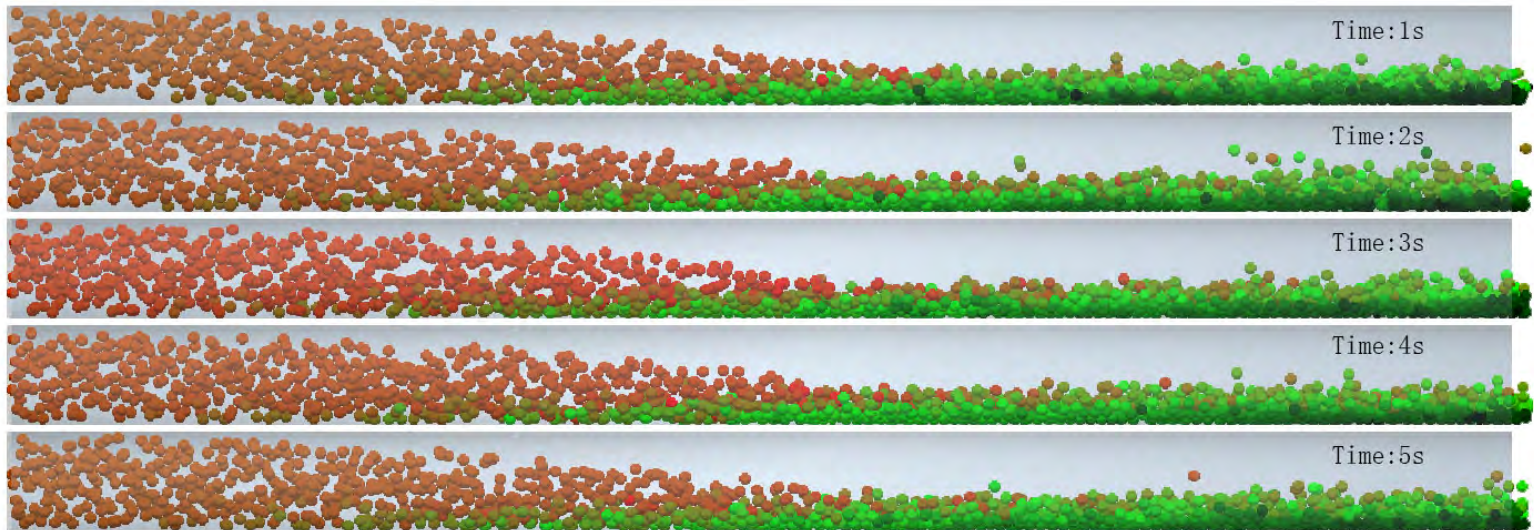
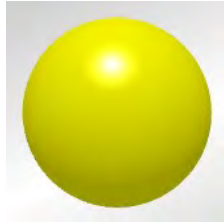
the maximum velocity points appear near the transition interfaces between different layers

## Non-spherical coarse particles in slurry transport



Heteromorphic / non-spherical Coarse-particles

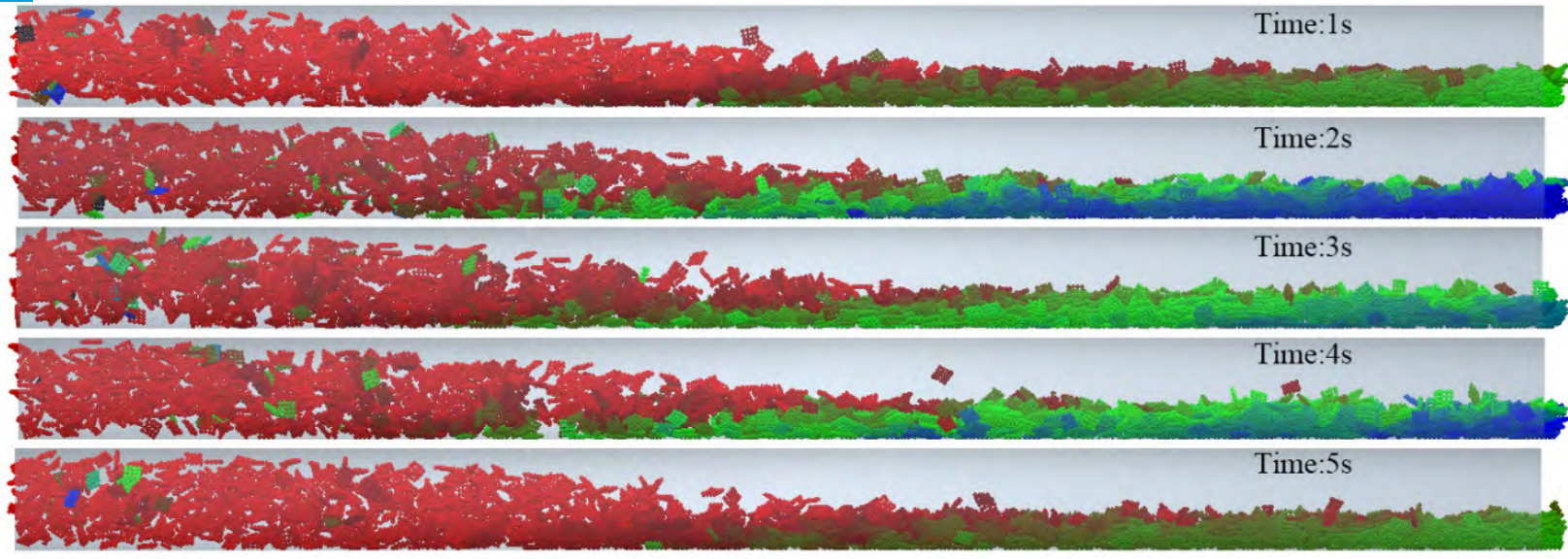
# Non-spherical coarse particles in slurry transport



The sliding flow state of spherical coarse-particles at line speed (8m/s)

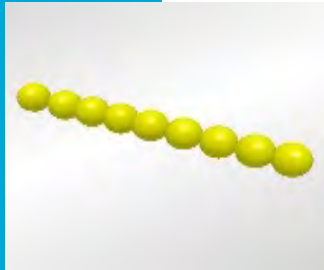


# Non-spherical coarse particles in slurry transport



The sliding bed flow regime of flatty coarse-particles at line speed (8m/s)

# Non-spherical coarse particles in slurry transport



The blockage of long coarse-particles at line speed (**8m/s**): flocculating + interlocking

## Conclusion

In this study, the CFD-DEM coupling numerical simulation method is used to analyze the flow characteristics and flow transition process of coarse particles under different line speeds

CFD-DEM coupling can present the flow regimes of slurry transport for coarse particles very well



- SLDV matches well with DHLLDV
- LDV shows a certain error with DHLLVD



Long shaped particles is the biggest threat to flow assurance

The authors appreciate the help from Mr. Robert Ramsdell.

Thank you very much!

